

## Low Attenuation Optical Fiber

### Field of the Invention

The present invention relates to low-attenuation optical fibers suitable for wavelength-division-multiplexing (WDM) optical transmission systems.

### Background of the Invention

Vigorous studies have been given on techniques to increase the capacity of optical-fiber transmission with optical fibers.

It is believed that a growth of optical transmission capacity requires the optical fibers for the optical transmission to enable single-mode transmission at the operating wavelength, because the groupings of different speeds of optical signals in various modes can induce mode dispersion inevitably in the propagation through an optical fiber. As a result, the signal waveforms can decay or warp.

Consequently, the single-mode fiber (SMF) was started in use, having a zero-dispersion wavelength around  $1.3 \mu\text{m}$ . At the zero-dispersion wavelength, the fiber was able to have a transmission distance of scores of kilometers, and a transmission capacity of hundreds of M b p s (megabits per second).

In the meantime, the least transmission loss in optical fiber takes place at  $1.55 \mu\text{m}$  of wavelength, where a dispersion-shifted fiber (DSF) with a zero-dispersion wavelength of  $1.55 \mu\text{m}$  or thereabout was developed. This optical fiber enabled the optical transmission optical transmission with a capacity of several gigabits per second around  $1.55 \mu\text{m}$  of wavelength. The same single-mode fibers were laid in long-distance optical transmission routes each with a capacity of several G bit/s in a  $1.55 \mu\text{m}$  wavelength band.

### Summary of the Invention

A purpose of the present invention is to provide low-attenuation fibers, or specifically, a low-attenuation fiber which comprises:

A dispersion  $D$  of 2.0 to 14.0 ps/nm/pkm in a wavelength range of 1530 to 1565nm in absolute value,

A transmission loss of 0.25dB/km or less under the standard atmospheric conditions, wherein the transmission loss at 1550nm and/or 1520nm in wavelength is made not to

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exceed 0.24dB, as a result of being exposed to an atmosphere composed substantially of hydrogen under the ordinary atmospheric pressure at ordinary temperature for a certain period. The standard atmospheric conditions refer to definitions in JISC0010, Section 5 and are made up of ordinary temperature ( $25 \pm 10^\circ\text{C}$ ), ordinary relative humidity (25-75%) and ordinary atmospheric pressure (86 - 106kPa). In addition, the certain period need to be no less than a time lapse in which hydrogen penetrates the midmost/core of an optical fiber. In effect, the hydrogen penetration is represented by at least 0.03dB/km of loss increase around  $1.24 \mu\text{m}$ .

#### Detailed Description

The latter half of the 1980s discovered a transmission loss increase in an optical fiber in which hydrogen molecules, from a hydrogen gas ( $\text{H}_2$ ) trapped in the cable, had broken. On analysis, the loss increase was assignable to absorption peaks in the transmission-loss spectrum, which hydrogen molecules had induced in the optical fiber. Hydrogen-induced absorption peaks emerge around  $1.24 \mu\text{m}$ , and at  $1.52 \mu\text{m}$  and on the longer-wavelength side. The absorption peaks at  $1.52 \mu\text{m}$  and the longer wavelength will have an adverse impact on the optical transmission around  $1.55 \mu\text{m}$ , firsthand, for instance, as described in ECOC '86, pp7-10, by Ogai et al.

Concurrently, in terms of  $1.31 \mu\text{m}$  transmission SMF and  $1.55 \mu\text{m}$  transmission DSF, assorted R& D approaches were made to prevent the hydrogen-induced loss increase, from the aspect of fabrication technique or fiber coating material. Yet for example, optical-fiber cables for terrestrial application were usually filled with a filling compound, without a threat of seriously trapping a gaseous hydrogen.

Accordingly, no argument over hydrogen-proof treatment (resistance to hydrogen) today takes place as described in Bellcore-GR-20-Core issue 2, July 1998, Section 6. 6. 9 "the generic specification in the United States," for example

In the recent years, in search for more capacities of optical transmission systems, the designs of wavelength division multiplexing (WDM) have been studied and developed in dead earnest, while volumes of studies on the optical fibers optimal for WDM optical transmission have been underway.

From the angle of evading four-wave mixing, the optical fibers for WDM optical transmission systems are required to be unequipped with a zero-dispersion wavelength in their operating wavelength bands. In this context, a non-zero dispersion shifted fiber

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(NZDSF) has been developed, without any zero dispersion in the operating wavelength band. In general, NZDSFs are required to have even more complicated refractive-index (RI) profiles, than those of SMFs or DSFs, because they need to gear with additional requirements for a large effective core area ( $A_{eff}$ ), a reduced dispersion slope, etc. to provide for high-density WDM (DWDM) optical transmission.

Complicated RI profile designs of NZDSFs accompany a propensity to induce minute glassmaking flaws in optical fibers, along with irksome process control.

Although NZDSFs are in use to cover a broad wavelength band including  $1.55 \mu m$ , no hydrogen-proof treatment techniques were then disclosed to the public.

In the recent years, cables to shroud optical fibers have structurally been reviewed and improved. In fact, optical fiber cables are shifting in great numbers from a compound-filled type to a dry-core type which contains a water absorbent material in the cable instead of a filling compound. The filling-compound free cable fabrication is far less toilsome (not required to wipe clean the cables). Also the filled cables could hardly be enhanced in fire resistance, but filling-compound free (dry-type) cables can readily be attached with enhanced fire resistance. A sample dry-core type of optical fiber cable is described in USP No. 5,422,973.

The dry-core type contains a water absorbent material in the cable to block out lengthwise, water penetration, which contacts wet, swells and dams off the water. But then, the water absorbent material has an action to lead in ambient humidity (moisture), even without any cable damage or opening, and poses a threat of allowing the trapped wet (absorbed ambient moisture) to react with component metals inside the cable, where hydrogen ions emerge. Accordingly, even optical fibers for terrestrial cables need to be considered about their hydrogen-proof treatment.

For instance, USP No. 6,131,415 describes an optical fiber with a thought of hydrogen-proof performance (hydrogen resistance), and a technique for suppressing the hydroxyl-ion concentration in an optical fiber to reduce the transmission loss at 1385nm. In particular, the present patent owner, Lucent Technologies, discloses in "Catalog Allwave," certain information about a required design concept of hydrogen-proof performance (hydrogen resistance) of optical fibers for metropolitan use.

Moreover, USP Nos. 5,838,866 and 6,128,928 each describe an optical fiber with a thought of hydrogen resistance. Each fiber is designed to be equipped with hydrogen resistance by making the (inner) clad contain germanium to a degree to raise its

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refractive index, not in substance.

However, USP No. 6,131,415 remarks on no more than a technique for suppressing the loss increase at 1385nm, arising out of absorption peaks of hydroxyl ions, without any remarks on the loss increase at 1520nm, due to the absorption peaks of hydrogen ions.

Moreover, none of the techniques in USP Nos. 6,131,415, 5,838,866 and 6,128,928 involve any additives to bring on substantial shifts in the refractive-index profile in each clad region. Thus, these three patents are expected to aim for characteristic improvements in "SMF" or the equivalent, but not NZDSF for WDM optical transmission systems.

The present invention is designed to provide hydrogen-proof optical fibers with moderate dispersions in a wavelength band between 1530 and 1564nm and transmission losses remaining almost constant over time.

Claim 1 of the present invention recites a low attenuation optical fiber which falls within 2-14 ps/nm/km in absolute value of dispersion over the wavelength range of 1530-1565nm and no more than 0.25dB/km of transmission loss at 1550nm of wavelength at ordinary temperature and relative humidity, and still remains no more than 0.25dB/km of transmission loss at 1550nm of wavelength even after its being long-enough exposed under ordinary atmospheric pressure consisting substantially of hydrogen.

Claim 2 of the present invention recites a low attenuation optical fiber which falls within 2-14 ps/nm/km in absolute value of dispersion over the wavelength range of 1530-1565nm and no more than 0.25dB/km of transmission loss at 1550nm of wavelength at ordinary temperature and relative humidity, and still remains no more than 0.25dB/km of transmission loss at 1520nm of wavelength even after its being long-enough exposed under ordinary atmospheric pressure consisting substantially of hydrogen.

Claim 3 of the present invention recites a low attenuation optical fiber based on Claim 1 or Claim 2, which further comprises a dispersion slope of no more than 15ps/nm<sup>2</sup>km over the wavelength band of 1530-1565nm, a PSD of no more than 5ps. km at a wavelength of 1550nm and a loss increase of no more than 40dB/km in a bending radius of 20mm.

Claim 4 of the present invention recites a low attenuation optical fiber based on Claim 3,

which further comprises  $90 \mu\text{m}$  of A eff.

Claim 5 of the present invention recites a low attenuation optical fiber based on Claim 3, which further comprises a dispersion slope of  $0.04\text{--}0.08\text{ps/nm}^2\text{km}$  over the wavelength band of  $1530\text{--}1565\text{nm}$ , an absolute value of dispersion of  $6\text{--}10\text{ps/nm/km}$  over the wavelength band of  $1530\text{--}1565\text{nm}$  and an A eff of  $40\text{--}70 \mu\text{m}$ .

Building blocks of the present invention as claimed up to now can make optical fibers suitable for the WDM optical transmission in a wavelength band of  $1530\text{--}1565\text{nm}$ .

The numerical limitations in the Claims are rounded in a method as authorized, for instance, by ASTM E29.

#### [Embodiment Model]

An embodiment of the present invention is explained with drawings from now onward.

Fig. 1 is a sketchy sample RI profile for a low-attenuation optical fiber of the present invention. Fig. 1 shows the midmost (core) region 1 and a clad 5, between which a first annular region 2, a second annular region 3 and a third annular region are located. The maximum refractive indices (RI) in the core, first, second and third regions 1, 2, 3 and 4 are larger than in the clad 5. The first annular region 2 is lower in refractive index than clad 5.

Fig. 2 shows a second sample of the RI profiles which an optical fiber of the embodiment may have. The profile in Fig. 2 have the midmost (core) region 1 and a clad 5, between which a first annular region 2, a second annular region 3 and a third annular region are located. The maximum refractive indices (RI) in the core, first, second and third regions 1, 2, 3 and 4 are larger than in the clad 5. Refractive indices in the, first, second and third regions, 2, 3 and 4, are lower than in the clad 5.

Notably, the RI profiles in Figs 1 and 2 are simply samples to which low-attenuation fibers of the present invention are not limited, in RI profile, provided that any RI profiles regarded as accordant with the present invention can be accepted.

In this embodiment, optical fibers are designed to have an absolute value of dispersion  $= 2\text{ps/nm/km} \leq |D| \leq 14\text{ps/nm/km}$  over the wavelength ( $\lambda$ ) range of  $1530\text{nm} \leq \lambda \leq 1565\text{nm}$ . It is because, in the wavelength ( $\lambda$ ) range of  $1530\text{nm} \leq \lambda \leq 1565\text{nm}$ , a four wave mixing impact is undesirably large at an absolute value of dispersion:  $|D|$  less than  $2\text{ps/nm/km}$ ; and, cumulative dispersions might unfavorably be combined to make high-density WDM optical transmission impracticable in the designed transmission

routes (systems), at an absolute value of dispersion:  $|D|$  more than 14ps/nm/km.

In contrast to similar conventional cases, the embodiment is characterized in that an optical fiber as based on the present invention and as long-enough exposed under a ordinary atmospheric pressure consisting substantially of hydrogen at ordinary temperature, can never exceed 0.25dB/km in transmission loss at 1550nm. The designed characteristic results from a fact of optical fibers with transmission losses in excess of 0.25dB/km regarded as undesirable at 1520 or 1550nm for long-distance WDM transmission, even with their having been long-enough exposed to a hydrogen atmosphere. Here, the ordinary atmospheric pressure consisting substantially of hydrogen means to yield an effect equivalent to a 100% hydrogen atmosphere; an atmosphere of at 90% hydrogen is desirable, if the remainder, 10% or less, is air. The long-enough exposed means a time lapse enough to allow hydrogen to reach the core of an optical fiber. Practically, it is when a loss increase of at least 0.03dB/km is determined at 1.24  $\mu$ m.

Considering the requirements for fiber characteristics in a wavelength band of 1530-1565nm, a range of dispersion of more than 0.15ps/nm/km is undesirable, because of its making dispersions vary greatly from wavelength to wavelength in WDM optical transmission; a polarization mode dispersion (PMD) of more than 0.5ps/ $\sqrt{\text{km}}$  is undesirable, because of its inducing a mass of polarization dispersion to disable WDM optical transmission; a bending loss increase of more than 40dB/m is undesirable, because of its inducing variations in transmission loss in optical fiber cables.

In addition, more than 90  $\mu\text{m}^2$  of  $A_{\text{eff}}$  in a wavelength range of 1530-1565nm is undesirable, because of its making the bending loss increase grow in volume hardly allowing cabling the optical fibers. Less than 40  $\mu\text{m}^2$  of  $A_{\text{eff}}$  is undesirable, because of its being more likely to induce nonlinear phenomena. In particular, more than 70  $\mu\text{m}^2$  of  $A_{\text{eff}}$ , which would be a factor in disagreeing with other characteristic requirements, ought to be studied out, against discrete system specifications in practice.

Here, the effective area ( $A_{\text{eff}}$ ) is defined with reference to Opt. Lett., Vol. 19, No. 4, pp 257-259 (Feb. 115, 1994).

A slope of dispersion, which would preferably be minimized, could be a factor in disagreeing with other characteristic requirements, if reduced to less than 0.04ps/nm<sup>2</sup>/km, and should be studied out, against discrete system specifications in practice, as to choice to less than 0.04ps/nm<sup>2</sup>/km. Conversely, more than 0.08ps/nm<sup>2</sup>/km

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of dispersion slope, with a propensity to risk the application to high-density WDM optical transmission, would preferably be studied out, against discrete system specifications in practice, as to choice to more than 0.08ps/nm<sup>2</sup>/km.

In terms of absolute values of dispersion, a four-wave mixing effect would arise below 6ps/nm/km and cumulative dispersions would risk the application to high-density WDM optical transmission above 10ps/nm/km. Design values of dispersion should preferably be set up, in view of discrete virtual system specifications.

In conclusion, considering the above details, it is preferable to opt for 40-70  $\mu$  m<sup>2</sup> of Aeff, 0.04 -0.08ps/nm<sup>2</sup>/km of dispersion slope range, and 6-10 ps/nm/km of absolute value of dispersion, in a wavelength band of 1530-1565nm.

#### [Embodiment]

Optical fibers were made to be equipped with refractive index (RI) profiles in Figs 1 and 2, underwent hydrogen-proof treatment and hydrogen-proof test, and served to demonstrate the present invention.

To name but a few, the hydrogen-proof treatments include a method of superficially etching in-process preforms in USP No. 6,131,415, a method of treating optical fibers in a heated heavy-hydrogen atmosphere (Deutrium, D2) in European Patent Application No. 0673895A2. Introducing the hydrogen-proof treatment into the production line, more safety and less process change are the most important items to be considered. After the result in studying the condition of the hydrogen-proof treatment, we found that the hydrogen-proof treatment under ordinary atmospheric pressure at ordinary temperature could provide sufficient hydrogen resistance for the NZDSFs.

In reality, a 3km-long coated optical fiber was led and held, for about 3 hours, in a treatment tank charged with D2 (heavy hydrogen) at almost ordinary temperature. Notably, more than two hours of remaining in a D2 atmosphere will produce a substantially constant effect, subject to a fiber length of 3 kilometers, where the hydrogen atmosphere does not need to be heated, but can produce a sufficient effect even at ordinary temperature as described in the Japanese Patent Publication. However, the holding time in a hydrogen atmosphere is required to be longer as the fiber under treatment becomes longer.

In the hydrogen-proof test, a 3km-long coated optical fiber was led and held, for six hours, in a test chamber charged with H2 at one pressure of an atmosphere and

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ordinary temperature; and the test chamber was recharged with nitrogen or air at ordinary temperature and the fiber was tested for transmission loss after dozens of hours. Here, more than four (4) hours of holding time in a hydrogen atmosphere will produce an almost constant effect, subject to a fiber length of three (3) kilometers. However, the holding time in a hydrogen atmosphere is required to be longer as the fiber under treatment becomes longer.

Pre/post hydrogen-proof treatment transmission losses (dB/km) are presented in Table 1, resulting from 20 sample pieces per embodiment, and consist of the discrete worst values.

Note: Measures (units) are as follows:

Dispersion: ps/nm/km

Dispersion slope: ps/nm/km

PMD: ps. km

Loss increase, 20mm in bend diameter: dB/m

A eff:  $\mu m^2$

Values of dispersion, dispersion slope are the maximums in 1530 - 1565nm.

Other values are taken at a wavelength of 1550nm.

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Table 1

|              | RI<br>profile | Dispersion<br>(ps/nm/km) | Dispersion<br>Slope<br>(ps/nm <sup>2</sup> /km) | PMD<br>(ps. Km) | Bend loss<br>(dB/m) | A eff<br>( $\mu$ m <sup>2</sup> ) | 1.55 $\mu$ m loss (dB/km) |           | 1.52 $\mu$ m loss (dB/km) |           |
|--------------|---------------|--------------------------|---|-----------------|---------------------|-----------------------------------|---------------------------|-----------|---------------------------|-----------|
|              |               |                          |   |                 |                     |                                   | pre-test                  | post-test | pre-test                  | post-test |
| Embodiment 1 | Fig.1         | 11                       | 0.05  | 0.03            | 1                   | 53                                | 0.213                     | 0.224     | 0.220                     | 0.228     |
| Embodiment 2 | Fig.1         | 9                        | 0.06  | 0.08            | 5                   | 56                                | 0.201                     | 0.215     | 0.209                     | 0.218     |
| Embodiment 3 | Fig.1         | 7                        | 0.06  | 0.09            | 6                   | 56                                | 0.205                     | 0.217     | 0.213                     | 0.224     |
| Embodiment 4 | Fig.2         | 5                        | 0.07  | 0.12            | 15                  | 57                                | 0.209                     | 0.221     | 0.218                     | 0.227     |
| Reference 1  | Fig.1         | 9                        | 0.06  | 0.08            | 5                   | 56                                | 0.201                     | 0.268     | 0.209                     | 0.396     |
| Reference 2  | Fig.2         | 5                        | 0.07  | 0.12            | 15                  | 57                                | 0.209                     | 0.277     | 0.218                     | 0.420     |

Table 1 reveals that hydrogen-proof optical fibers have been suppressed to be less than 0.25 dB/km in transmission loss, even after each hydrogen-proof test in a hydrogen (D2) atmosphere. In contrast, References 1 and 2 without hydrogen-proof treatment, turn out to be more than 0.25 dB/km in transmission loss after hydrogen-proof test.

Moreover, it is verified that hydrogen-proof optical fibers with other RI profiles (e.g., single peaked, stepped or W pattern) than those in Figs 1 and 2, have incurred no increase in transmission loss in a hydrogen-proof test.

As unveiled in the above descriptions, the present invention has superior effects to facilitate the fabrication of optical fibers suited to the WDM optical transmission in a wavelength band of 1530-1565nm.

#### Brief Description of the Drawings

Fig. 1 is a sample sketchy RI profile for a low attenuation optical fiber as an embodiment in the present invention.

Fig. 2 is a second sample sketchy RI profile for a low attenuation optical fiber as an embodiment in the present invention.

#### Legend

- 1 Core region
- 2 1st annular region
- 3 2nd annular region
- 4 3rd annular region
- 5 Clad

#### Abstract of the Disclosure

A low attenuation optical fiber which falls within 2-14 ps/nm/km in absolute value of dispersion over the full wavelength range of 1530-1565nm and no more than 0.25dB/km of transmission loss at 1550nm of wavelength at ordinary temperature and relative humidity, and still remains no more than 0.25dB/km of transmission loss at 1550nm or 1520 nm after its being long-enough exposed under ordinary atmospheric pressure consisting substantially of hydrogen; and which further comprises a polarization mode dispersion (PMD) of no more than 0.5ps/ $\sqrt{\text{km}}$  at a wavelength of 1550nm and a loss increase of no more than 40dB/km in a bending radius of 20mm.